

High-Power Polarization-Engineered GaN/AlGa_N/GaN HEMTs Without Surface Passivation

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Abstract—In this paper, a high-power GaN/AlGa_N/GaN high electron mobility transistor (HEMT) has been demonstrated. A thick cap layer has been used to screen surface states and reduce dispersion. A deep gate recess was used to achieve the desired transconductance. A thin SiO₂ layer was deposited on the drain side of the gate recess in order to reduce gate leakage current and improve breakdown voltage. No surface passivation layer was used. A breakdown voltage of 90 V was achieved. A record output power density of 12 W/mm with an associated power-added efficiency (PAE) of 40.5% was measured at 10 GHz. These results demonstrate the potential of the technique as a controllable and repeatable solution to decrease dispersion and produce power from GaN-based HEMTs without surface passivation.

Index Terms—GaN, microwave power field effect transistors (FETs), MODFETs, passivation, RF-dispersion.

I. INTRODUCTION

AS A PROMISING candidate for future microwave power devices, GaN-based high electron mobility transistors (HEMTs) have attracted much research interest [1]. A combination of high breakdown field, high sheet charge density and high electron velocity in AlGa_N/GaN HEMTs gives great potential for high power high frequency applications. Output power density of 11.2 W/mm at 10 GHz has been reported recently [2]. However, many GaN-based power HEMTs suffer from current collapse during large signal operation at high frequency, usually referred as “dc-to-radio frequency (RF) dispersion”. Slow response of surface traps is believed to be one of the major contributing factors [3]. Si_N passivation has been used to suppress this problem [4], but reproducibility of breakdown voltage, gate leakage, and effectiveness of dispersion elimination is undependable. Recently, solutions to the dispersion problem have been addressed at epitaxial level [5]–[7]. The development of the GaN/AlGa_N/GaN HEMT is one of these efforts [7]. A thick GaN cap was introduced in

the access region to reduce surface potential fluctuations from affecting device performance, thus decreasing dispersion. Very promising power data have been shown recently utilizing these structures [7], namely, 3.4 W/mm with PAE of 32% at drain bias of 15 V at 10 GHz without Si_N passivation on sapphire. However, the maximum drain bias that could be applied to these devices during power measurements was limited by high gate leakage and low breakdown voltage. A reduction in gate leakage and an increase in breakdown voltage are needed to obtain higher power. In this paper we propose a general solution to these problems. By depositing a SiO₂ insulating layer against the gate recess sidewall on the drain side, gate leakage current decreased and breakdown voltage increased. Due to the effective dispersion control and increased breakdown voltage, a record output power density was achieved without passivation.

II. DEVICE STRUCTURE

The device structures studied in this paper were grown by metal-organic chemical vapor deposition (MOCVD) on both sapphire and SiC substrates. The epitaxial structure (shown in Fig. 1) consisted of a semi-insulating Fe-doped GaN buffer layer [8], followed by a 0.7-nm AlN interfacial layer, a 40-nm Al_{0.22}Ga_{0.78}N layer, a 10-nm graded Al_xGa_{1-x}N layer ($x = 0.22-0$) doped by Si ($8 \times 10^{18} \text{ cm}^{-3}$) and a 250-nm unintentionally doped (UID) GaN cap layer. Room temperature sheet charge density and Hall mobility were $8 \times 10^{12} \text{ cm}^{-2}$ and $2000 \text{ cm}^2/\text{V}\cdot\text{s}$, respectively.

Using charge control analysis, the ability of surface potential to modulate the channel charge is inversely proportional to the distance between surface and channel. The 250-nm GaN cap layer is used to increase the surface-channel distance to a value where surface potential fluctuations no longer effectively modulate the channel charge. Dispersion from surface states is therefore reduced or eliminated. The graded AlGa_N layer is Si-doped to compensate the negative polarization charge and prevent hole accumulation. The thin AlN layer is utilized to remove alloy disorder scattering and improve mobility [9].

To investigate the contribution of the recessed sidewalls to the gate leakage current, two devices were processed. The first had a full gate metal coverage on the recess sidewalls, while the other had spacing ($\sim 0.3-0.4 \mu\text{m}$) between the gate metal and the recess sidewalls. The latter showed one order of magnitude lower gate leakage current. This suggested that most of the gate leakage was not through the bottom of the recessed trench,

Manuscript received August 14, 2003; revised November 5, 2003. This work was supported by the Office of Naval Research through the CANE MURI program under Contract N00014-01-1-0764. The review of this letter was arranged by Editor T. Mizutani.

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Digital Object Identifier 10.1109/LED.2003.821673

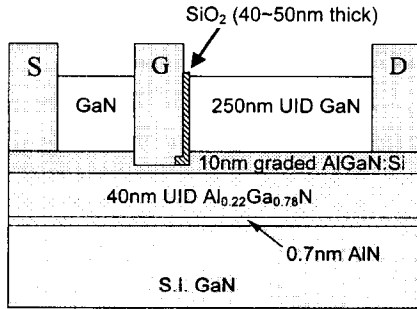


Fig. 1. Schematic of the proposed GaN/AlGaIn/GaN HEMT structure. The thin SiO₂ insulating layer helps reducing the gate leakage and improving the breakdown voltage.

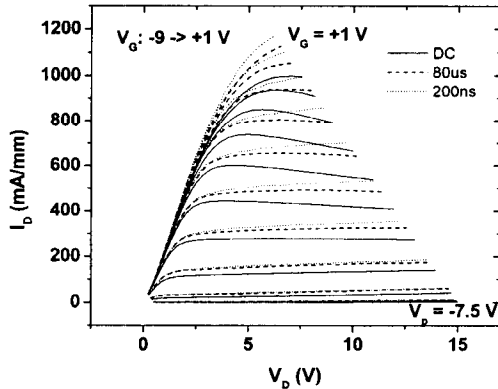


Fig. 2. DC and pulsed I - V characteristics of an unpassivated GaN/AlGaIn/GaN HEMT on sapphire. Device dimension: $0.7 \times 150 \mu\text{m}^2$. No dispersion was observed up to 200 ns.

but through the sidewalls. Moreover, because the gate-drain bias voltage is much larger than the gate-source bias voltage, the sidewall of the drain side is the major current path of the gate leakage current.

To decrease this leakage, a thin SiO₂ layer (40–50 nm) was introduced to cover the sidewall of the drain side and eliminate the leakage current path [10]. Fig. 1 shows the schematic cross section of the device. Device fabrication was similar to conventional AlGaIn/GaN HEMTs. Self-aligned deep recesses before ohmic and gate metallizations were needed to obtain ohmic contacts, reasonable pinch-off voltage ($-5 \sim -7$ V) and transconductance (~ 200 mS/mm). SiO₂ was deposited prior to the gate metallization. During e-beam SiO₂ evaporation, the sample was tilted so that the drain sidewall was covered and the coverage of the gate region remained as small as possible. Gate length was $0.7 \mu\text{m}$ and gate width was $150 \mu\text{m}$ ($2 \times 75 \mu\text{m}$). This method can be extended to smaller gate-length devices by using some other SiO₂ deposition techniques (e.g., PECVD SiO₂ deposition with dry-etching of SiO₂ on the etched gate surface).

III. DEVICE PERFORMANCE

The introduction of the SiO₂ layer improved gate leakage current and breakdown voltage while retaining dispersion removal. Fig. 2 shows the dc and pulsed current–voltage (I - V) characteristics of an unpassivated device on a sapphire substrate. At pulse width of 200 ns, no dispersion was observed when the

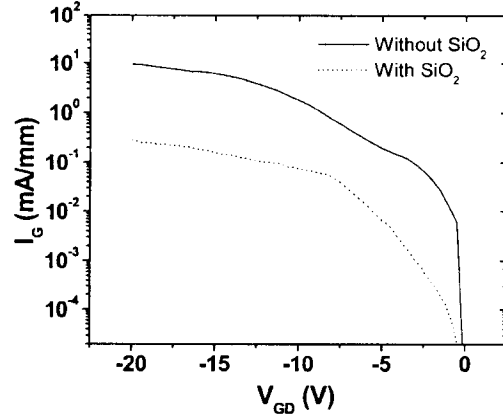


Fig. 3. Gate-drain leakage current densities for devices with and without SiO₂ sidewall coverage. For the SiO₂ covered devices, the insulator thickness on the sidewall was about 50 nm. More than one order of magnitude reduction in gate leakage current was achieved by the introduction of SiO₂.

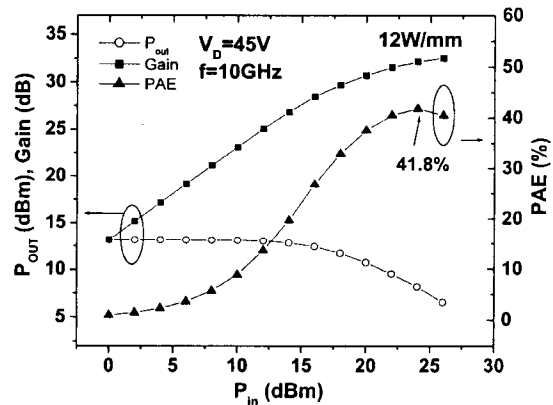


Fig. 4. Power performance of an unpassivated $0.7 \mu\text{m} \times 150 \mu\text{m}$ GaN/AlGaIn/GaN HEMT on SiC substrate at 10 GHz. Bias conditions were $V_D = 45$ V and $I_D = 270$ mA/mm. An output power density of 12 W/mm with an associated PAE of 40.5% was achieved.

SiO₂ coverage under the gate was minimized and a current density of 1.2 A/mm was obtained. Gate leakage was decreased by one to two orders of magnitude, from 10 to 0.3 mA/mm at a gate-drain bias of -20 V, as shown in Fig. 3. The destructive two terminal breakdown voltage was more than 90 V, compared to 35 V for devices without the SiO₂ layer. This allowed the application of higher drain bias. For unpassivated devices on sapphire substrate, a maximum drain bias of 25 V could be applied, compared to a drain bias of 15 V without SiO₂. Uncooled continuous-wave (CW) power measurements were performed. A saturated power density of 4.8 W/mm with peak PAE of 33% was obtained for devices on sapphire substrate at 10 GHz. Similar devices grown on SiC substrate were also processed. A record output power density of 12 W/mm with an associated PAE of 40.5% at a drain bias of 45 V at 10 GHz was achieved without SiN passivation, as shown in Fig. 4. At peak PAE point of 42%, a power density of 11 W/mm was obtained. This is due to the effective dispersion control and the application of high drain bias.

Preliminary investigation of the effect of SiO₂ coverage on the bottom of the gate recess was carried out. Different tilt an-

gles were used during SiO₂ deposition to apply varying SiO₂ coverage under the gate. The coverage length was characterized by atomic force microscopy (AFM). Though there was a small increase in dispersion with increasing coverage under the gate (studied to a maximum coverage of 0.3 μm), the effect was small enough such that similar microwave performance was observed from these devices. It showed that the process has acceptable tolerance to the SiO₂ deposition step.

IV. CONCLUSION

In conclusion, an improved GaN/AlGaIn/GaN HEMT was demonstrated. A thin SiO₂ layer was introduced to cover the gate recess sidewall of the drain side. The gate leakage current was reduced and breakdown voltage increased compared to devices without SiO₂. An output power density of 12 W/mm with an associated PAE of 40.5% was achieved without SiN passivation at 10 GHz with a drain bias of 45 V. This is the highest output power density ever reported for GaN devices. This promising result demonstrates the great potential of this technique as a controllable and repeatable solution for decreasing dispersion and producing power without surface passivation.

ACKNOWLEDGMENT

The authors would like to thank P. Hansen for the useful discussion.

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